# Redefining the Microwave Plasma Mediated CO<sub>2</sub> Reduction

# Efficiency Limit: The role of O-CO<sub>2</sub> Association

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### Abstract

Reduction of  $CO_2$  to CO for sustainable fuel production is studied in high temperature (>3500 K) microwave plasma. Raman scattering and chemical kinetics modelling reveal chemistry rates with spatial resolution that explain previously reported peak energy efficiency values of 50%. The necessary product quenching is established by fast transport in the core, at frequencies of  $10^5 \text{ s}^{-1}$ , facilitating rapid mass and energy transfer between products and feedstock  $CO_2$ . Moreover, the resulting chemical non-equilibrium yields additional  $CO_2$  dissociation in O- $CO_2$  association, a reaction responsible for up to 45% of CO production. Three different thermal chemistry sets are invoked to qualitatively confirm this picture. It is shown how these lack predictive accuracy in the high gas temperature regime studied, which indicates that new  $CO_2$  chemistry rate coefficients are highly desirable. Improving reactor design with the identified enhancement mechanisms in mind can increase efficiency up to the newly defined thermal limit of 70%.

### TOC graphic



*Introduction:* In our transition towards a circular economy,  $CO_2$  reduction powered by renewable energy is recognized as an opportunity to produce sustainable carbon feedstocks for the synthesis of fuels and chemicals<sup>1–3</sup>.  $CO_2$  reduction with high-temperature microwave plasmas (>3500 K) is a promising technology, as recent experimental results show conversions up to 80% and maximum energy efficiencies up to 50%<sup>4,5</sup>. This maximum experimental energy efficiency is close to the theoretical efficiency limit (~52%) of thermal  $CO_2$  splitting with no CO losses in back-reactions and in which  $O_2$  is formed by O-recombination (i.e. with absolute quenching)<sup>4,6,7</sup>:

$$\begin{array}{ll} \text{CO}_2 \rightarrow \text{CO} + 0 & \text{R. 1} \\ 0 + 0 \rightarrow 0_2 & \text{R. 2} \end{array}$$

It has been hypothesized that this limit can be increased significantly by controlling the quenching trajectory of the atomic oxygen generated in R. 1. Association of O with  $CO_2$  yields an additional CO for each  $O_2$  which would increase the efficiency limit to  $70\%^{6,8}$  by valorizing the enthalpy of formation of nascent O atoms:

$$0 + CO_2 \rightarrow CO + O_2.$$
 R. 3

The mechanism is called super-ideal quenching<sup>9,10</sup>, but is yet to be demonstrated to contribute to the overall efficiency. Elucidating the importance of this reaction is the primary goal of this work.

In addition to thermal chemistry, vibrational activation and vibration-driven dissociation is generally assumed to be important in microwave plasmas<sup>7,9–15</sup>. It has been proposed as an explanation for early work with unparalleled energy efficiencies exceeding 80%<sup>12</sup>. However, recent investigations could not link vibrational-translational non-equilibrium with high performance <sup>8,16–18</sup>, instead in most CO<sub>2</sub> microwave plasma experiments thermal dissociation mechanisms are predominant <sup>6,8,14,19,20</sup>. Nevertheless, it is relevant to note that the vibration-driven mechanism also relies on R. 3 to complete the reaction scheme with highest efficiency.

Hence, insight in the recombination of O-atoms and the potential of its control is decisive for evaluation of the maximum performance of CO<sub>2</sub> conversion, in microwave plasma in particular, and in high temperature systems in general. This work succeeds for the first time in unravelling both the quenching mechanisms and reaction kinetics using an *in-situ* characterization of the chemical and physical state of the reactor. Raman scattering is used

to create maps of temperature (rotational and vibrational)<sup>16</sup> and composition (CO<sub>2</sub>, CO, O<sub>2</sub>,  $O)^{21}$ , with more details in the supporting information. The experimental data is interpreted with our 0D chemical kinetics model<sup>19</sup> to yield local species sources (and sinks). The global reactor productivity is obtained by integrating the local chemistry rates over the volume, which in turn elucidates the importance of O-radical induced CO<sub>2</sub> dissociation (R. 3) compared to the other chemical pathways.

This approach elucidates reaction pathways independent of the unknown flow field in the studied configuration. The rationale is that all locally determined chemical rates sum to the reactor integrated rate of those reactions. We therefore divide the reactor into a fine grid composed of control volumes, in which the effect of complex, local transport phenomena are inherently captured. Notwithstanding this independence of flow in the analysis is the strong dependence of the eventual reactor performance on details of transport and flow, which will affect measured distributions of temperature and composition.

The analysis also relies on accurate knowledge of rate constants. Multiple datasets exist in literature, and some of their rate constants disagree by several orders of magnitude; the rate constant of the reaction  $CO_2 + M \rightarrow CO + O + M$  can differ by an order of magnitude, while that of  $O_2$  recombination can vary by four orders of magnitude. The most widely used kinetic data are rates: (i) from Butylkin<sup>22</sup>, developed at the time of the early experiments and used by e.g. Wolf et al.<sup>6</sup>, Van den Bekerom et al.<sup>8</sup> and Den Harder et al.<sup>4</sup>; (ii) from GRI-MECH<sup>23</sup> developed for combustion and used by e.g. Viegas et al.<sup>19</sup>; and (iii) derived from the NIST chemical kinetics database, used by e.g. Kozak et al.<sup>13</sup>, Koelman et al.<sup>11</sup> and Pietanza et al.<sup>24</sup> It is important to note that all sets reasonably approach the equilibrium composition (through Gibbs free energy minimization) at long integration times (see the supporting information).

The structure of this letter is as follows. First, we map rovibrational temperatures and composition in a large cross-section of the reactor. Second, this data is used to quantify local chemistry timescales as well as the main reaction pathways of CO production and O-quenching. Thus, we illustrate the potential of super-ideal quenching to increase energy efficiency in CO<sub>2</sub> microwave plasma.

*Results:* Four experiments with varying process conditions were pressures of 60 and 120 mbar, with flows of pure  $CO_2$  of 10 and 20 slm all at a fixed input power of 1000 W. The

apparent plasma volume decreases with pressure from a diffuse appearance at 60 mbar to a thin and bright filament at 120 mbar due to plasma contraction<sup>25</sup>, an effect that coincides with increasing performance<sup>4,26</sup>. Flow does not affect the plasma shape but changes the quenching trajectory, resulting in improved efficiency. While the precise mechanisms are still unknown, Wolf et al.<sup>6</sup> predicted increasing efficiency with increasing flow is a result of faster downstream cooling.



Figure 1: Plasma emission and spatially resolved Raman results of the 10 slm, 120 mbar, 1000 W plasma. The emission map is an overlay of total emission and 777 nm oxygen emission in the core. Black dots represent locations where Raman spectra are recorded. Cylindrical symmetry is assumed, and data is linearly interpolated between measurement points. Subsequent maps represent rotational temperature, CO<sub>2</sub> fraction, CO fraction, O<sub>2</sub> fraction and O fraction.

The Raman-derived temperature and composition measurements (Figure 1) are the basis for the characterization of transport and chemistry. The results illustrate the extreme temperature in which the reactor operates, with the plasma core reaching 6000 K. In this ultra-high temperature region, the majority of CO<sub>2</sub> is dissociated and CO concentration peaks at 50%. This observation is consistent with the predominance of the thermal CO<sub>2</sub> dissociation mechanism. Additionally, O<sub>2</sub> is largely absent in the plasma core, instead atomic oxygen reaches a fraction of almost 50%. Separate regions of O and O<sub>2</sub> formation are revealed, the maxima in these fractions are spatially offset by approximately 40 mm.

The supporting information includes results for the other tested conditions. Two main differences are observed with respect to Figure 1. (i) At lower pressure, power absorption is less concentrated, this follows from the broader temperature profile that peaks at a reduced

value of 3500-4000 K. Additionally, CO<sub>2</sub> is the majority species in the plasma core with concentration fractions above 50% throughout the reactor. (ii) Remarkably, the increased feed gas flowrate results in a larger penetration of products upstream of the plasma core. Consequently, the O<sub>2</sub> fraction peaks upstream of the core instead of downstream. This last finding hints at a flow reversal and recirculation as a result of the tangential gas injection<sup>6</sup>. In literature, plug-flow behavior is generally assumed in alike configurations<sup>4,6,8,10,13,20,24,27</sup>, which clearly oversimplifies core-exhaust transport.

We have measured vibrational temperatures in several key-positions in the reactor via vibrational Raman scattering: a radial scan at 0 mm and at 35 mm for 60 and 120 mbar, 10 slm. Measurements do not show any spectral signature of a vibrational non-equilibrium, neither between the different vibrational modes or with the gas/rotational temperature (see supplemental information). It confirms that a Boltzmann distribution can be used to evaluate the rotational and vibrational degrees of freedom.

Although no vibrational non-equilibrium is observed, a strong chemical non-equilibrium is present. For example, the 60 mbar core temperature is ~4000 K with CO<sub>2</sub> as majority species, while chemical equilibrium (often assumed for the core<sup>4,6,28</sup>) shows CO<sub>2</sub> fractions below 1% at this temperature. The supporting information contains additional details on the present chemical non-equilibrium for the conditions examined. Summarizing, because of the higher temperature, at higher pressure the strongest chemical non-equilibrium is present in the region surrounding the plasma core, whilst at lower pressure this chemical non-equilibrium occurs within the plasma core.

Deviations from chemical equilibrium are a result of the interplay between fast transport and chemistry. Invoking chemical kinetics modeling allows us to quantify the transport timescales by assuming steady state and a balance between transport and chemistry at each position, for each species *i*:

$$\frac{dn_i}{dt} = 0 = \sum_j S_{i,j} \pm v_i n_i. \qquad eq. 1$$

Here  $\frac{dn_i}{dt}$  is the temporal derivative of the species number density  $n_i$ , equal to zero due to steady state assumption.  $S_{i,j}$  is the chemistry source (or loss, if negative) rate of species i through reaction j. The replacement frequency  $v_i$  of species i is the inverse of the particle

transport loss time  $t_{ri}$ . The  $v_i n_i$  term can be positive or negative, depending on the sign of the chemistry term, where positive refers to supply of the species.

The chemistry rates  $S_{i,j}$  are assessed with our OD model<sup>19</sup> invoking the three aforementioned thermal chemistry sets. The model also assesses charged particle kinetics assuming an electron density profile that was recently measured in our lab under similar conditions<sup>25</sup>.



Figure 2:  $CO_2$  replacement frequencies ( $v_{CO_2}$ ) for the different discharge conditions as calculated by the plasma chemical kinetics model and GRI-MECH rate constants. Positive chemistry frequencies are shown in blue and negative transport frequencies in red. White denotes  $-1 < v_{CO_2} < 1 \text{ s}^{-1}$ , where the system is near chemical equilibrium.

Figure 2 shows the spatial distribution of  $v_{CO_2}$ , the transport frequency of CO<sub>2</sub>, as obtained with the GRI-MECH rate constants, for each pressure and gas flow setting. The supplemental information discusses the replacement frequency of other particles. The regions where CO<sub>2</sub> is formed by chemistry (blue) have a very small chemistry time constant in all conditions, the fastest being of the order of  $10^{-1}$  s. This timescale is inconsequential compared with the bulk-transport timescale of the reactor which is one to two orders of magnitude shorter<sup>4,6</sup>. In the plasma core, CO<sub>2</sub> is supplied by transport and consumed by chemistry (red) with a timescale of ~ $10^{-5}$  s in the hottest regions. On average, timescales of  $10^{-3}$  s at 60 mbar and  $10^{-4}$  s at 120 mbar are observed in the plasma core, similarly as in Wolf et al.<sup>6</sup> Using the Kozak and Butylkin schemes result in slightly different transport values, but the general observations in terms of chemistry remain the same.

The global reactor productivity equals the integration over the local chemistry rates over the total volume. The quenching of O-atoms and the different production and loss mechanisms of CO can be directly identified in this way. This analysis is only valid if the complete chemically active portion of the reactor is captured. Chemistry timescales at x = -50 or x = 100 mm are  $10^{0}$ - $10^{-1}$  s, i.e. orders of magnitude lower than in the core or surrounding regions and at least an order of magnitude below average reactor residence times<sup>4,6</sup>. Hence, we conclude there is no notable role of chemistry outside the probed volume. Numerically we calculate the global chemical activity as:

$$\frac{dR_{i,tot}}{dt} = \sum_{\bar{x}} \frac{dR_{i,loc}(r,z)}{dt} V(r,z). \qquad eq. 2$$

Here  $\frac{dR_{i,tot}}{dt}$  is the reactor-integrated rate of reaction *i*,  $\frac{dR_{i,loc}(r,z)}{dt}$  is the local rate of reaction *i* at spatial coordinate *r*, *z* and *V*(*r*, *z*) is the volume corresponding to the cylinder element at this coordinate. The reaction rates are calculated over a fine grid using linearly interpolated experimental data.

Figure 3 compares the result for the main reactions and for three chemistry sets. The CO and O production rates through charged species chemistry are plotted separately. Those rates refer to, among others, direct electron impact dissociation, dissociative recombination, and dissociative attachment.



Figure 3: Reactor integrated rates using three kinetic schemes for low (left) and high (right) pressure. Error margins are propagated from experimental uncertainties in temperature and fractions (see supporting information).

While the absolute rates among the different chemistry sets can vary by more than an order of magnitude, qualitatively all chemistry sets are consistent: back-reactions re-forming  $CO_2$ are of minimal importance and charged particle chemistry only plays a role in providing dissociation at low pressure. At higher pressures, termal chemistry dominates due to contraction, high temperatures and increasing collisionality. Combining the results of Figure 3 with the locally determined reaction rates elucidates the main dissociation pathways for the 120 mbar conditions: the high temperature core produces CO and O, while fast transport extracts these and provides fresh  $CO_2$ . The extracted O-atoms then recombine preferentially with  $CO_2$  to produce CO and  $O_2$ ; the rate of this reaction is of the same order of magnitude as other CO-producing reactions. These two distinct dissociation reactions are dominant in separate regions, the core, with T ~6000 K and surrounding the core, with T ~3000 K.

While the chemical kinetics sets are all in qualitative agreement, we obtain best quantitative agreement with the GRI-MECH set as shown in Figure 4. In this figure, we compare the total CO production with that measured by effluent Fourier Transform infrared (FTIR) absorption spectroscopy (top) and total power in chemistry with the input power (bottom). The total CO production is obtained by summing the rates of CO producing and consuming reactions of Figure 3. The total power consumed in chemical reactions is obtained the same way, but considering the enthalpy change of a reaction. The calculated power should be within the yellow area of Figure 4, the boundaries of which are given by the 1 kW input power and the power retained in stable products in the effluent, which reflects the true efficiency.



Figure 4: Comparison of reactor integrated CO production (d[CO]/dt) (top) and power consumption (bottom) compared with values measured in the effluent. Error margins are propagated from errors in reaction rates of Figure 3. Power is expected to be in the yellow area, which is between the total input power (1 kW) and the enthalpy in products retained at the FTIR.

The rates obtained with the Butylkin dataset overestimate CO production consistently and show, even beyond the error margins, a power consumption above 1000 W in the 120 mbar conditions. The Kozak and GRI-MECH schemes are similar in terms of CO production and power, although with the Kozak scheme, CO production from reaction R. 3 exceeds that of R. 1 at 120 mbar. This gives the Kozak scheme a physically unfeasible negative O-atom production rate: more O is consumed than produced. Based on these considerations we recommend using GRI-MECH rate constants, but also stress that a new evaluation of CO<sub>2</sub> rate constants at high temperature is necessary.

According to the results of Figure 3 and the GRI-MECH scheme, 68% of all O-atoms are lost in O+CO<sub>2</sub> association, thereby producing 45% of all CO in the conditions of Figure 1 (120 mbar,

10 slm, 1000 W). The other plasma conditions show similarly high values. The apparent importance of this reaction forces a redefinition of the thermal efficiency limit. The current 52% limit is based on absolute quenching<sup>4,6,7</sup>, whereas we have experimentally shown super-ideal quenching, and the underlying  $O+CO_2$  association reaction, to be a main  $CO_2$  dissociation mechanism. Given this, the efficiency limit of thermal  $CO_2$  splitting should be increased to 70%<sup>6,8</sup> to include the effective valorization of O-atoms through super-ideal quenching.

The results also underline the opportunity to surpass the 50% efficiency via optimization of residence times in both core and periphery. Just outside the plasma core, with temperatures decreasing, competing reaction kinetics can lead to (un)favorable utilization of the atomic oxygen. If the temperature falls below 2000 K and cooling is very fast, atomic O will preferentially recombine to O<sub>2</sub>. Conversely, if cooling is too slow, O + CO recombination would be favored<sup>6,10</sup>. The optimal temperature for preferential super ideal quenching is 3000 K, where the predicted thermal equilibrium composition is primarily composed of CO and O<sub>2</sub>. Therefore, to gain maximum utility from super-ideal quenching, the hot core of the plasma - the predominant source of atomic oxygen - should be surrounded by a cloak of gas maintained at 3000 K; this would create favorable reaction conditions and allow sufficient time for the relatively slow O + CO<sub>2</sub> reaction to occur.

*Conclusion*: We show that the high energy efficiency of the CO<sub>2</sub> microwave plasma is predominantly explained by thermal chemistry occurring within the plasma core, alongside a chemical non-equilibrium that facilitates super-ideal quenching of atomic oxygen. Steep temperature gradients drive fast core-periphery transport and mixing, thereby minimizing CO losses and optimizing O-utilization. Additionally, we find no evidence of a vibrational-translational non-equilibrium. This work therefore challenges the prevailing hypothesis that the vibrational dissociation mechanism is responsible for reported high performance.

Further reactor engineering can improve efficiency by increasing the chemical nonequilibrium surrounding the core. This increases CO formation outside the core through super-ideal quenching of oxygen atoms. Reaching this super-ideally quenched system requires precise control over temperature and residence time but opens a window to boost CO<sub>2</sub> reduction efficiency to 70%. **Acknowledgements:** This research received funding from the Netherlands Organization for Scientific Research (NWO) in the framework of the CO2-to-Products program with kind support from Shell, and the ENW PPP Fund for the top sectors. We are grateful to E. Langereis for his support in the design of schematics.

**Supporting Information Available:** Experimental details, comparison of thermal chemistry sets, spectral analysis, error analysis, additional results of rotational and vibrational Raman scattering, replacement frequencies and chemical non-equilibrium.

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